

# Lecture 06

## Velocity Propagation

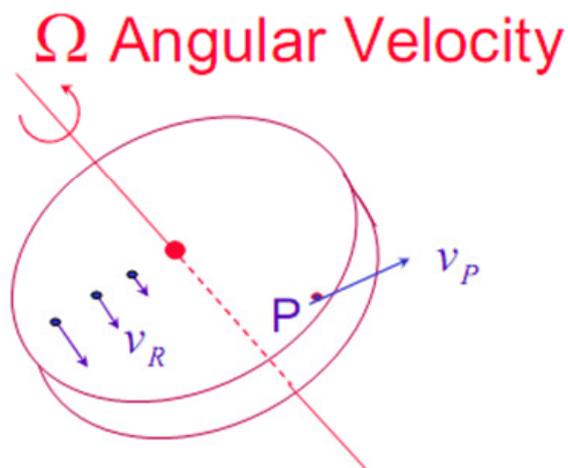
Acknowledgement :

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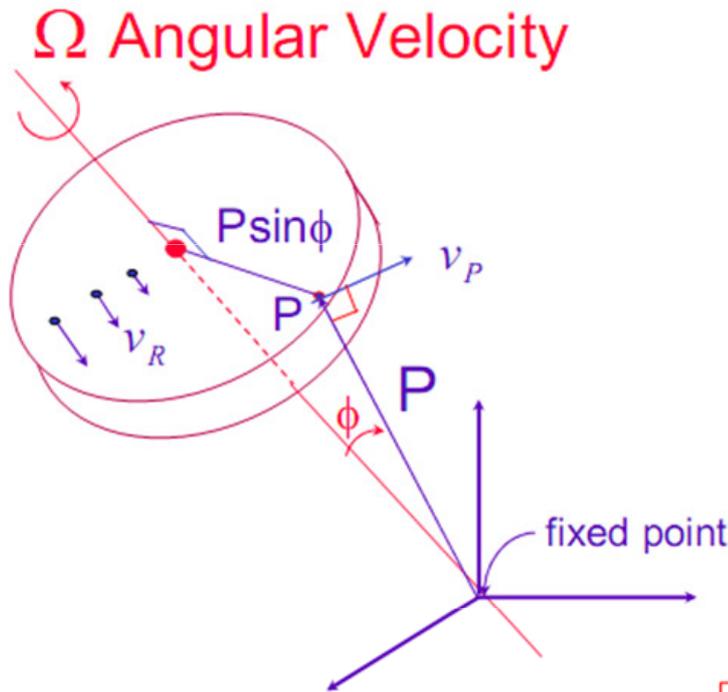
## Rotational Motion



$$v_P = ?$$

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# Rotational Motion



$v_P$  is proportional to:

- $\|\Omega\|$
- $\|P \sin \phi\|$

and

- $v_P \perp \Omega$
- $v_P \perp P$

$$v_P = \Omega \times P$$

Eg:  $\Omega = \langle 1, 3, 2 \rangle$ ,  $P = \langle -2, 0, 1 \rangle$

$\Omega \times P = \langle (3 \times 1), -(1 \times 1) + 2 \times 2, -(3 \times -2) \rangle$

$\Omega \times P = \langle 3, -5, 6 \rangle$

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# Cross Product Operator

$$a = \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix}, b = \begin{bmatrix} b_x \\ b_y \\ b_z \end{bmatrix}$$

$$c = a \times b \Rightarrow c = \hat{a}b$$

vectors  $\Rightarrow$  matrices

$a \times \Rightarrow \hat{a}$  : a skew-symmetric matrix

$$c = \hat{a}b = \begin{bmatrix} 0 & -a_z & a_y \\ a_z & 0 & -a_x \\ -a_y & a_x & 0 \end{bmatrix} \begin{bmatrix} b_x \\ b_y \\ b_z \end{bmatrix}$$

$$c = \hat{a}b$$

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# Cross Product Operator

$$v_P = \Omega \times P \Rightarrow v_P = \hat{\Omega}P$$

$\Omega \times \Rightarrow \hat{\Omega}$  : a skew-symmetric matrix

$$\Omega = \begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix}; P = \begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix}$$

$$v_P = \hat{\Omega}P = \begin{bmatrix} 0 & -\Omega_z & \Omega_y \\ \Omega_z & 0 & -\Omega_x \\ -\Omega_y & \Omega_x & 0 \end{bmatrix} \cdot \begin{bmatrix} P_x \\ P_y \\ P_z \end{bmatrix}$$

$$v_P = \hat{\Omega}P$$

Eg:  $\Omega = \langle 1, 3, 2 \rangle$ ,  $P = \langle -2, 0, 1 \rangle$

$$\Omega \times P = \hat{\Omega}P = \begin{bmatrix} 0 & -2 & 3 \\ 2 & 0 & -1 \\ -3 & 1 & 0 \end{bmatrix} \begin{bmatrix} -2 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 3 \\ -5 \\ 6 \end{bmatrix}$$

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# Linear and Angular Velocity

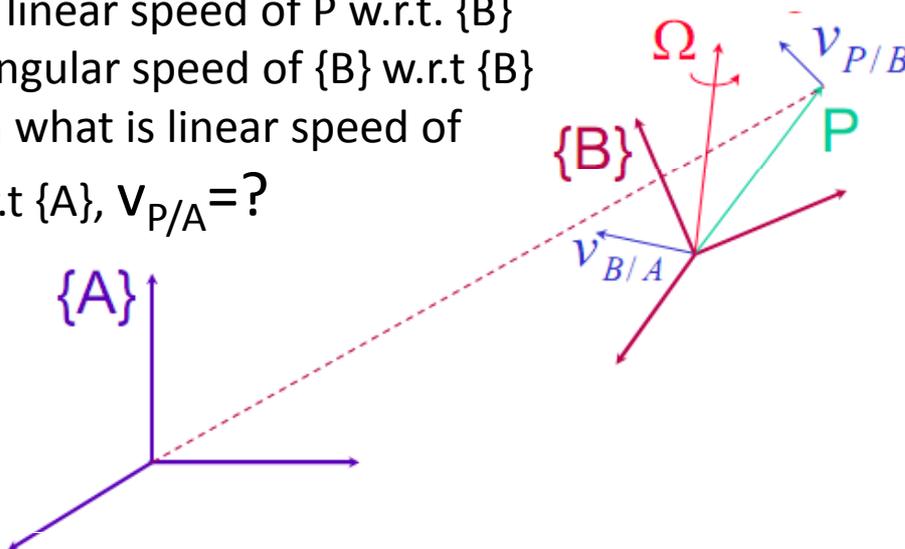
$v_{B/A}$  : linear speed of {B} w.r.t. {A}

$v_{P/B}$  : linear speed of P w.r.t. {B}

$\Omega$  : angular speed of {B} w.r.t {B}

Then what is linear speed of

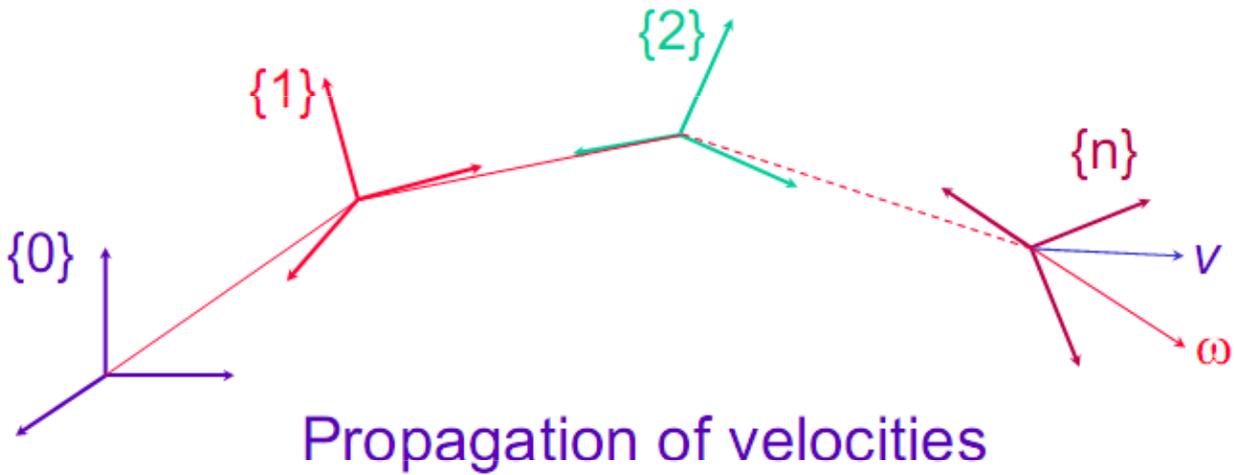
P w.r.t {A},  $v_{P/A} = ?$



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# Velocity Propagates from Base to End

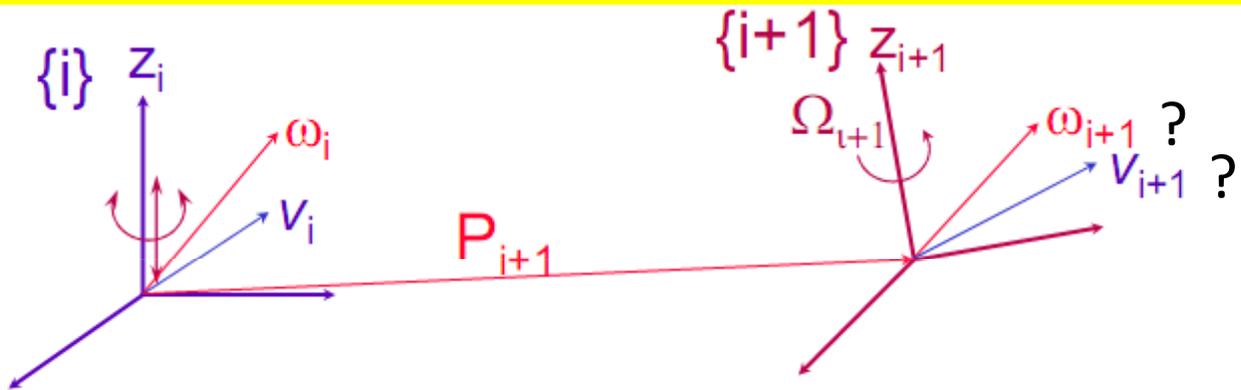
## Spatial Mechanisms



$\dot{x} \begin{cases} v : \text{linear velocity} \\ \omega : \text{angular velocity} \end{cases}$

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## Velocity Propagation from {i} to {i+1}

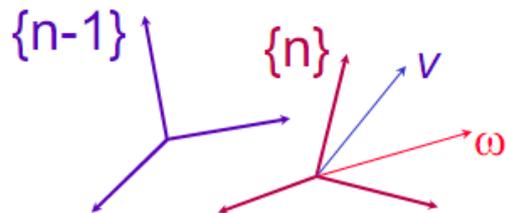


$${}^{i+1}\omega_{i+1} = {}^{i+1}R_i \cdot {}^i\omega_i + \dot{\theta}_{i+1} \cdot {}^{i+1}Z_{i+1}$$

$${}^{i+1}v_{i+1} = {}^{i+1}R_i \cdot ({}^i v_i + {}^i\omega_i \times {}^i P_{i+1}) + \dot{d}_{i+1} \cdot {}^{i+1}Z_{i+1}$$

$\Rightarrow {}^n\omega_n$  and  ${}^n v_n$

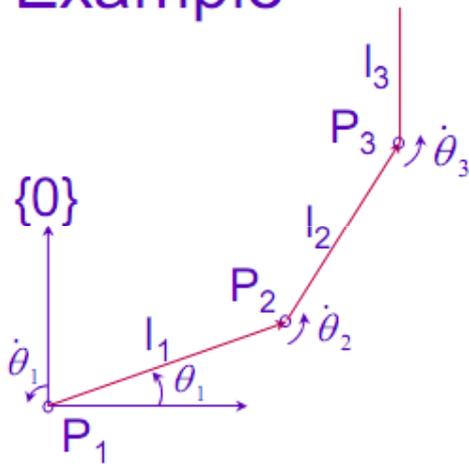
$$\begin{pmatrix} {}^0 v_n \\ {}^0 \omega_n \end{pmatrix} = \begin{pmatrix} {}^0 R_n & 0 \\ 0 & {}^0 R_n \end{pmatrix} \begin{pmatrix} {}^n v_n \\ {}^n \omega_n \end{pmatrix}$$



Computationally Complex because of frame transformation

# Tutorial

## Example



Fixed frame of reference {0}

$$v_{i+1} = v_i + \omega_i \times P_{i+1}$$

- $v_{P_1} = 0$        ${}^0\omega_1 = \dot{\theta}_1 \cdot {}^0Z_1$
- $v_{P_2} = v_{P_1} + \omega_1 \times P_2$
- $v_{P_3} = v_{P_2} + \omega_2 \times P_3$

w.r.t. {0}

$${}^0v_{P_2} = 0 + \begin{bmatrix} 0 & -\dot{\theta}_1 & 0 \\ \dot{\theta}_1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} l_1 \cdot c_1 \\ l_1 \cdot s_1 \\ 0 \end{bmatrix} = \begin{bmatrix} -l_1 \cdot s_1 \\ l_1 \cdot c_1 \\ 0 \end{bmatrix} \cdot \dot{\theta}_1$$

**Computationally efficient because of fixed frame of Ref. {0}**

$${}^0\omega_2 = {}^0\omega_1 + {}^0\dot{\theta}_2 \hat{z}_2 = \begin{bmatrix} 0 & 0 & (\dot{\theta}_1 + \dot{\theta}_2) \end{bmatrix}^T$$

$${}^0v_{P_3} = {}^0v_{P_2} + {}^0\omega_2 \times {}^0P_3$$

$$\begin{aligned} {}^0v_{P_3} &= \begin{bmatrix} -l_1 \cdot s_1 \\ l_1 \cdot c_1 \\ 0 \end{bmatrix} \cdot \dot{\theta}_1 + \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot (\dot{\theta}_1 + \dot{\theta}_2) \cdot \begin{bmatrix} l_2 \cdot c_{12} \\ l_2 \cdot s_{12} \\ 0 \end{bmatrix} \\ &= \begin{bmatrix} -l_1 \cdot s_1 \\ l_1 \cdot c_1 \\ 0 \end{bmatrix} \cdot \dot{\theta}_1 + \begin{bmatrix} -l_2 \cdot s_{12} \\ l_2 \cdot c_{12} \\ 0 \end{bmatrix} \cdot (\dot{\theta}_1 + \dot{\theta}_2) \end{aligned}$$

Angular velocity of P3 w.r.t {0}  $\uparrow$   
 2<sup>nd</sup> link w.r.t {0}  $\uparrow$

$${}^0 v_{P_3} = \underbrace{\begin{bmatrix} -(l_1 s_1 + l_2 s_{12}) & -l_2 s_{12} & 0 \\ l_1 c_1 + l_2 c_{12} & l_2 c_{12} & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{J_v} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix}$$

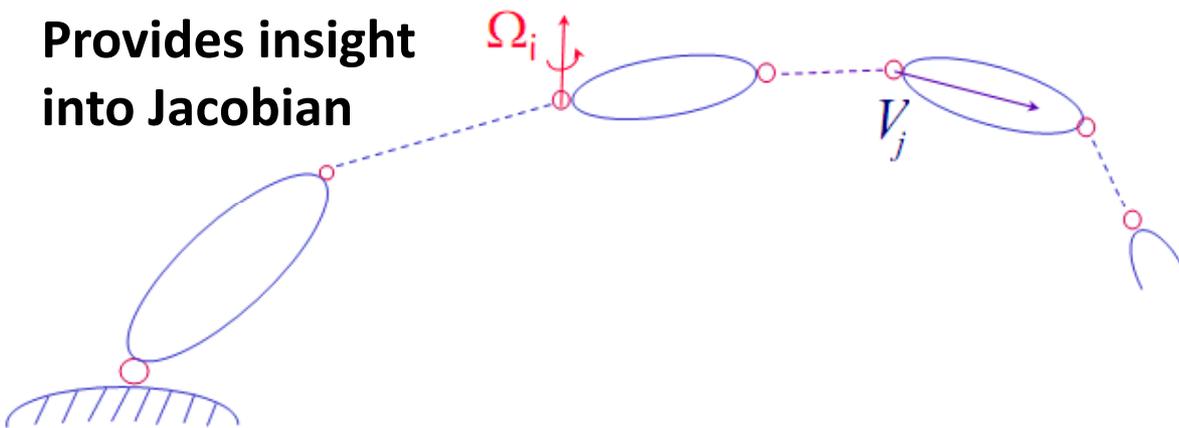
$${}^0 \omega_3 = \underbrace{\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}}_{J_\omega} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} \leftarrow {}^0 \omega_3 = {}^0 \omega_2 + {}^0 \dot{\theta}_3 \hat{z}_3 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3 \end{bmatrix}$$

$$\begin{pmatrix} v \\ \omega \end{pmatrix} = J \cdot \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{pmatrix}$$

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## The Jacobian (EXPLICIT FORM)

Provides insight  
into Jacobian



Revolute Joint  $\Omega_i = Z_i \dot{q}_i$

Prismatic Joint  $V_i = Z_i \dot{q}_i$

Describe how each joint contributes to  $V$  and  $\omega$  of the end-effector

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# The Jacobian (EXPLICIT FORM)

Neglect co-ordinate transformation

Effector      Prismatic      Revolute

Linear Vel:  $V_j$        $\Omega_i \times P_{in}$

Angular Vel: none       $\Omega_i$

Effector Linear Velocity

Effector Angular Velocity

Every joint contributes to  $v$   
Only R joints contribute to  $\omega$

$$v = \sum_{i=1}^n [\epsilon_i V_i + \bar{\epsilon}_i (\Omega_i \times P_{in})] \iff V_i = Z_i \dot{q}_i$$

$$\omega = \sum_{i=1}^n \bar{\epsilon}_i \Omega_i \iff \Omega_i = Z_i \dot{q}_i$$

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Contributes only if the last joint is prismatic

$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n})] \dot{q}_1 + \dots + [\epsilon_{n-1} Z_{n-1} + \bar{\epsilon}_{n-1} (Z_{n-1} \times P_{(n-1)n})] \dot{q}_{n-1} + \epsilon_n Z_n \dot{q}_n$$

$$v = [\epsilon_1 Z_1 + \bar{\epsilon}_1 (Z_1 \times P_{1n}) \quad \epsilon_2 Z_2 + \bar{\epsilon}_2 (Z_2 \times P_{2n}) \quad \dots] \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$

$v = J_v \dot{q}$

There is an easier way to determine  $J_v$  using T

$$\omega = \bar{\epsilon}_1 Z_1 \dot{q}_1 + \bar{\epsilon}_2 Z_2 \dot{q}_2 + \dots + \bar{\epsilon}_n Z_n \dot{q}_n$$

$$\omega = [\bar{\epsilon}_1 Z_1 \quad \bar{\epsilon}_2 Z_2 \quad \dots \quad \bar{\epsilon}_n Z_n] \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$

$\omega = J_\omega \dot{q}$

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# Jacobian of a 6dof manipulator

All rotary manipulator (eg. Puma560)

Without frame transformation

$$\begin{pmatrix} \mathbf{v} \\ \boldsymbol{\omega} \end{pmatrix} = \begin{bmatrix} \mathbf{z}_1 \times \mathbf{P}_{16} & \mathbf{z}_2 \times \mathbf{P}_{26} & \mathbf{z}_3 \times \mathbf{P}_{36} & \mathbf{z}_4 \times \mathbf{P}_{46} & \mathbf{z}_5 \times \mathbf{P}_{56} & \mathbf{z}_6 \times \mathbf{P}_{66} \\ \mathbf{z}_1 & \mathbf{z}_3 & \mathbf{z}_3 & \mathbf{z}_4 & \mathbf{z}_5 & \mathbf{z}_6 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

With co-ordinate transformation

$$\begin{pmatrix} {}^0\mathbf{v} \\ {}^0\boldsymbol{\omega} \end{pmatrix} = \begin{bmatrix} {}^0_1\mathbf{R}(\mathbf{z}_1 \times \mathbf{P}_{16}) & {}^0_2\mathbf{R}(\mathbf{z}_2 \times \mathbf{P}_{26}) & {}^0_3\mathbf{R}(\mathbf{z}_3 \times \mathbf{P}_{36}) & {}^0_4\mathbf{R}(\mathbf{z}_4 \times \mathbf{P}_{46}) & {}^0_5\mathbf{R}(\mathbf{z}_5 \times \mathbf{P}_{56}) & {}^0_6\mathbf{R}(\mathbf{z}_6 \times \mathbf{P}_{66}) = 0 \\ {}^0_1\mathbf{R}\mathbf{z}_1 & {}^0_2\mathbf{R}\mathbf{z}_3 & {}^0_3\mathbf{R}\mathbf{z}_3 & {}^0_4\mathbf{R}\mathbf{z}_4 & {}^0_5\mathbf{R}\mathbf{z}_5 & {}^0_6\mathbf{R}\mathbf{z}_6 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

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# Jacobian of a 6dof manipulator

Stanford Schinman Arm (RRPRRR)

Without frame transformation

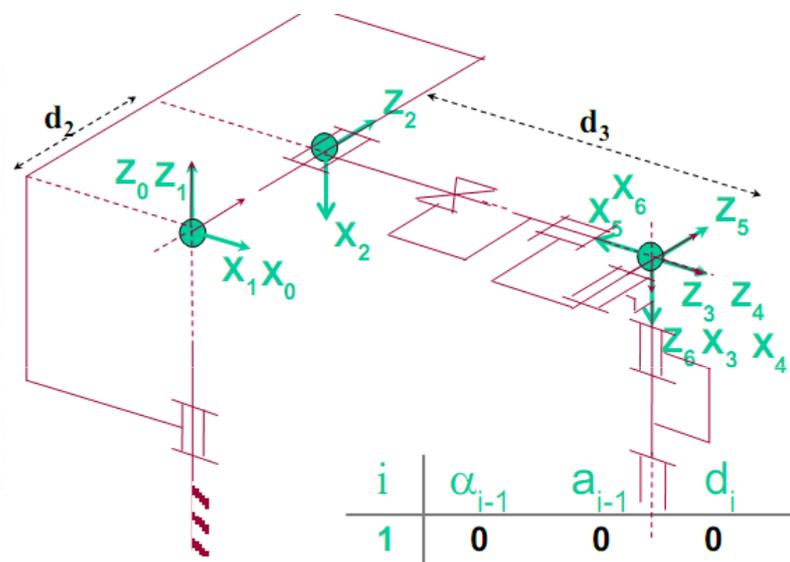
$$\begin{pmatrix} \mathbf{v} \\ \boldsymbol{\omega} \end{pmatrix} = \begin{bmatrix} \mathbf{z}_1 \times \mathbf{P}_{16} & \mathbf{z}_2 \times \mathbf{P}_{26} & \mathbf{z}_3 & \mathbf{z}_4 \times \mathbf{P}_{46} = 0 & \mathbf{z}_5 \times \mathbf{P}_{56} = 0 & \mathbf{z}_6 \times \mathbf{P}_{66} = 0 \\ \mathbf{z}_1 & \mathbf{z}_3 & 0 & \mathbf{z}_4 & \mathbf{z}_5 & \mathbf{z}_6 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

With co-ordinate transformation

$$\begin{pmatrix} {}^0\mathbf{v} \\ {}^0\boldsymbol{\omega} \end{pmatrix} = \begin{bmatrix} {}^0_1\mathbf{R}(\mathbf{z}_1 \times \mathbf{P}_{16}) & {}^0_2\mathbf{R}(\mathbf{z}_2 \times \mathbf{P}_{26}) & {}^0_3\mathbf{R}\mathbf{z}_3 & 0 & 0 & 0 \\ {}^0_1\mathbf{R}\mathbf{z}_1 & {}^0_2\mathbf{R}\mathbf{z}_2 & 0 & {}^0_4\mathbf{R}\mathbf{z}_4 & {}^0_5\mathbf{R}\mathbf{z}_5 & {}^0_6\mathbf{R}\mathbf{z}_6 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \dot{q}_5 \\ \dot{q}_6 \end{bmatrix}$$

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# Stanford Scheinman Arm



$i$	$\alpha_{i-1}$	$a_{i-1}$	$d_i$	$\theta_i$
1	0	0	0	$\theta_1$
2	-90	0	$d_2$	$\theta_2$
3	90	0	$d_3$	0
4	0	0	0	$\theta_4$
5	-90	0	0	$\theta_5$
6	90	0	0	$\theta_6$

$$\begin{pmatrix} v \\ \omega \end{pmatrix} = J = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix}$$

$$J = \begin{pmatrix} \mathbf{R} & \mathbf{R} & \mathbf{P} & \mathbf{R} & \mathbf{R} & \mathbf{R} \\ Z_1 \times P_{13} & Z_2 \times P_{23} & Z_3 & 0 & 0 & 0 \\ \hline Z_1 & Z_2 & 0 & Z_4 & Z_5 & Z_6 \end{pmatrix}_{17}$$

## Matrix $J_v$ (direct differentiation)

$$v = \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{pmatrix} = \dot{x}_P = \underbrace{\frac{\partial x_P}{\partial q_1} \cdot \dot{q}_1 + \frac{\partial x_P}{\partial q_2} \cdot \dot{q}_2 + \dots + \frac{\partial x_P}{\partial q_n} \cdot \dot{q}_n}_{3 \times n}$$

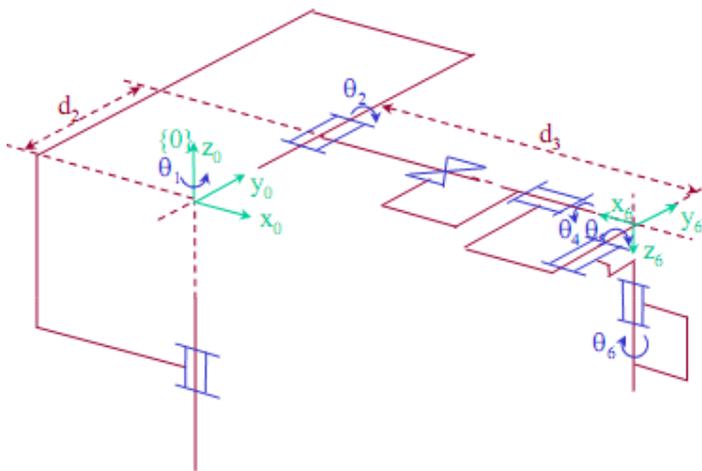
$$J_v = \begin{pmatrix} \frac{\partial x_P}{\partial q_1} & \frac{\partial x_P}{\partial q_2} & \dots & \frac{\partial x_P}{\partial q_n} \end{pmatrix}$$

$${}^0_n T = \begin{bmatrix} x \\ y \\ z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# SCA Jacobian from HTMs

$$\begin{array}{c}
 \frac{\partial {}^0T(:4)}{\partial q_1} \quad \frac{\partial {}^0T(:4)}{\partial q_2} \quad {}^0\hat{Z}_3 \\
 J = \begin{pmatrix}
 \mathbf{R} & \mathbf{R} & \mathbf{P} & \mathbf{R} & \mathbf{R} & \mathbf{R} \\
 Z_1 \times P_{13} & Z_2 \times P_{23} & Z_3 & 0 & 0 & 0 \\
 Z_1 & Z_2 & 0 & Z_4 & Z_5 & Z_6
 \end{pmatrix} \\
 {}^0\hat{Z}_1 \quad {}^0\hat{Z}_2 \quad {}^0\hat{Z}_4 \quad {}^0\hat{Z}_5 \quad {}^0\hat{Z}_6 \\
 {}^0_1R(:3) \quad {}^0_2R(:3) \quad {}^0_4R(:3) \quad {}^0_5R(:3) \quad {}^0_6R(:3)
 \end{array}$$

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$i$	$\alpha_{i-1}$	$a_{i-1}$	$d_i$	$\theta_i$
1	0	0	0	$\theta_1$
2	-90	0	$d_2$	$\theta_2$
3	90	0	$d_3$	0
4	0	0	0	$\theta_4$
5	-90	0	0	$\theta_5$
6	90	0	0	$\theta_6$

$${}^{i-1}T_i = \begin{bmatrix}
 c\theta_i & -s\theta_i & 0 & a_{i-1} \\
 s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1} d_i \\
 s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1} d_i \\
 0 & 0 & 0 & 1
 \end{bmatrix}$$

Forward Kinematics:  ${}^0T_N = {}^0T_1 {}^1T_2 \dots {}^{N-1}T_N$

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$${}^0_1T = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^1_2T = \begin{bmatrix} c_2 & -s_2 & 0 & 0 \\ 0 & 0 & 1 & d_2 \\ -s_2 & c_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^2_3T = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & -d_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

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$${}^3_4T = \begin{bmatrix} c_4 & -s_4 & 0 & 0 \\ s_4 & c_4 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^4_5T = \begin{bmatrix} c_5 & -s_5 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -s_5 & -c_5 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^5_6T = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

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$$\begin{aligned}
{}^0_1T &= \begin{bmatrix} c_1 & -s_1 & \boxed{0} & 0 \\ s_1 & c_1 & \boxed{0} & 0 \\ 0 & 0 & \boxed{1} & 0 \\ 0 & 0 & \boxed{0} & 1 \end{bmatrix} \begin{matrix} {}^0R(:3) \\ \\ \\ \end{matrix} \\
{}^0_2T &= \begin{bmatrix} c_1c_2 & -c_1s_2 & \boxed{-s_1} & -s_1d_2 \\ s_1c_2 & -s_1s_2 & \boxed{c_1} & c_1d_2 \\ -s_2 & -c_2 & \boxed{0} & 0 \\ 0 & 0 & \boxed{0} & 1 \end{bmatrix} \begin{matrix} {}^0R(:3) \\ \\ \\ \end{matrix} \\
{}^0_3T &= \begin{bmatrix} c_1c_2 & -s_1 & \boxed{c_1s_2} & c_1d_3s_2 - s_1d_2 \\ s_1c_2 & c_1 & \boxed{s_1s_2} & s_1d_3s_2 + c_1d_2 \\ -s_2 & 0 & \boxed{c_2} & d_3c_2 \\ 0 & 0 & \boxed{0} & 1 \end{bmatrix} \begin{matrix} {}^0R(:3) \\ \\ \\ \end{matrix}
\end{aligned}$$

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$${}^0_4T = \begin{bmatrix} c_1c_2c_4 - s_1s_4 & -c_1c_2s_4 - s_1c_4 & \boxed{c_1s_2} & c_1d_3s_2 - s_1d_2 \\ s_1c_2c_4 + c_1s_4 & -s_1c_2s_4 + c_1c_4 & \boxed{s_1s_2} & s_1d_3s_2 + c_1d_2 \\ -s_2c_4 & s_2s_4 & \boxed{c_2} & d_3c_2 \\ 0 & 0 & \boxed{0} & 1 \end{bmatrix} \begin{matrix} {}^0R(:3) \\ \\ \\ \end{matrix}$$

$${}^0_5T = \begin{bmatrix} X & X & \boxed{-c_1c_2s_4 - s_1c_4} & c_1d_3s_2 - s_1d_2 \\ X & X & \boxed{-s_1c_2s_4 + c_1c_4} & s_1d_3s_2 + c_1d_2 \\ X & X & \boxed{s_2s_4} & d_3c_2 \\ 0 & 0 & \boxed{0} & 1 \end{bmatrix} \begin{matrix} {}^0R(:3) \\ \\ \\ \end{matrix}$$

$${}^0_6T = \begin{bmatrix} X & X & \boxed{c_1c_2c_4s_5 - s_1s_4s_5 + c_1s_2s_5} & c_1d_3s_2 - s_1d_2 \\ X & X & \boxed{s_1c_2c_4s_5 + c_1s_4s_5 + s_1s_2c_5} & s_1d_3s_2 + c_1d_2 \\ X & X & \boxed{-s_2c_4s_5 + c_5c_2} & d_3c_2 \\ 0 & 0 & \boxed{0} & 1 \end{bmatrix} \begin{matrix} {}^0R(:3) \\ \\ \\ \end{matrix}$$

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## Stanford Scheinman Arm Jacobian

$${}^0J = \begin{pmatrix} \frac{\partial^0 x_P}{\partial q_1} & \frac{\partial^0 x_P}{\partial q_2} & \frac{\partial^0 x_P}{\partial q_3} & 0 & 0 & 0 \\ {}^0Z_1 & {}^0Z_2 & 0 & {}^0Z_4 & {}^0Z_5 & {}^0Z_6 \end{pmatrix}$$

$$\begin{bmatrix} -c_1 d_2 - s_1 s_2 d_3 & c_1 c_2 d_3 & c_1 s_2 & 0 & 0 & 0 \\ -s_1 d_2 + c_1 s_2 d_3 & s_1 c_2 d_3 & s_1 s_2 & 0 & 0 & 0 \\ 0 & -s_2 d_3 & c_2 & 0 & 0 & 0 \\ 0 & -s_1 & 0 & c_1 s_2 & -c_1 c_2 s_4 - s_1 c_4 & c_1 c_2 c_4 s_5 - s_1 s_4 s_5 + c_1 s_2 c_5 \\ 0 & c_1 & 0 & s_1 s_2 & -s_1 c_2 s_4 + c_1 c_4 & s_1 c_2 c_4 s_5 + c_1 s_4 s_5 + s_1 s_2 c_5 \\ 1 & 0 & 0 & c_2 & s_2 s_4 & -s_2 c_4 s_5 + c_5 c_2 \end{bmatrix}$$

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## Jacobian in a Frame

### Vector Representation

$$J = \begin{pmatrix} \frac{\partial x_P}{\partial q_1} & \frac{\partial x_P}{\partial q_2} & \dots & \frac{\partial x_P}{\partial q_n} \\ \overline{\epsilon}_1 \cdot Z_1 & \overline{\epsilon}_2 \cdot Z_2 & \dots & \overline{\epsilon}_n \cdot Z_n \end{pmatrix}$$

In  $\{0\}$

$${}^0J = \begin{pmatrix} \frac{\partial^0 x_P}{\partial q_1} & \frac{\partial^0 x_P}{\partial q_2} & \dots & \frac{\partial^0 x_P}{\partial q_n} \\ \overline{\epsilon}_1 \cdot {}^0Z_1 & \overline{\epsilon}_2 \cdot {}^0Z_2 & \dots & \overline{\epsilon}_n \cdot {}^0Z_n \end{pmatrix}$$

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## J in Frame {0}

$${}^0Z_i = {}^0R {}^iZ_i; \quad {}^iZ_i = Z = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

**3<sup>rd</sup> colomn in  ${}^0R$**

$${}^0J = \begin{pmatrix} \frac{\partial}{\partial q_1} ({}^0x_P) & \frac{\partial}{\partial q_2} ({}^0x_P) & \dots & \frac{\partial}{\partial q_n} ({}^0x_P) \\ \overline{\epsilon}_1 \cdot ({}^0R.Z) & \overline{\epsilon}_2 \cdot ({}^0R.Z) & \dots & \overline{\epsilon}_n \cdot ({}^0R.Z) \end{pmatrix}$$

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